

Tomlinson Group of Companies – PROPOSED ASPHALT PLANT Stormwater Management Design Brief

8205 COUNTY ROAD 2, NAPANEE, ONTARIO

Prepared for: Tomlinson Group

Prepared by: Groundwork Engineering Limited

Project No. GW-20019

Original Report Date June 2020 Revised: December 2020



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1.0 Introduction

Groundwork Engineering Limited (GWEL) has been retained by R.W. Tomlinson (Owner) to prepare a Stormwater Management design brief to support a zoning bylaw amendment to allow for an asphalt plant on the site.

The site is a vacant lot that has been partially stripped down to bedrock. Areas not stripped remain heavily treed. The site is located at 8205 County Road 2, Napanee, which can be legally described as Part 2 of Lot 21 Concession 7, Town of Greater Napanee, County of Lennox and Addington.

2.0 Existing Site Conditions

The site topography is gently sloping from the north to the southwest. The site has an existing gravel access road along the west side. The access road is on a shared unopened road allowance. A drainage ditch on the east side of the access road outfalls to the roadside ditch parallel to Highway 2. A portion of the site bordering the existing quarry has been stripped down to bedrock and is being used to store excess material. The remainder of the site is heavily treed.

The site currently has no stormwater management. The stormwater runs naturally via sheet flow to three (3) different receiving points, the existing quarry to the north, the neighboring property to the west, and to a roadside ditch parallel to Highway 2 via a ditch along the entrance road. The site is located at a high point with little to no off-site drainage entering the site.

The adjoining quarry lands to the north have a stormwater management plan that includes quantity and quality control. The stormwater outlets to the roadside ditch along Palace Road. The plan is approved by the Ministry of Environment, Conservation and Parks (MECP) under an Environmental Compliance Approval (ECA) for Industrial Sewage Works (No. 1967-BPKLCB).

3.0 Stormwater Management

The report deals with the stormwater management for the developed portion of the property identified as an asphalt plant site only.

Post-development stormwater management protects receiving watercourses. Post-development stormwater flows must meet pre-development flows. The Quinte Conservation Authority (QCA) requires quantity and quality control. It is expected that the "enhanced" level (80%) Total Suspended Solids (TSS) removal will be achieved for all runoff from the newly developed portion of the site.

Using the MECP guidelines, the development has been designed to provide adequate stormwater management control and improve runoff quality. It is our goal to utilize grassed swales and a wet pond to reduce TSS and improve the runoff quality. The pond will use an orifice and a rectangular weir as Inlet Control Devices (ICD) to discharge stormwater at less than the controlled pre-development flow rate.





3.1 Pre-Development Drainage Areas

Existing stormwater drainage areas are illustrated in the Pre-development drainage area drawing provided in Appendix A. The existing site is divided into three (3) stormwater drainage areas with the neighboring property, the existing quarry to the north of the subject property, and a municipally owned drainage ditch located parallel to Highway 2 being the ultimate receiving course. The drainage areas were determined using 3D analysis of a topographical survey completed by GWEL and CRCA LiDAR data. The drainage areas are valid as of the date of the survey.

Pre-development drainage areas are illustrated in Appendix A.

Drainage area P-1 is approximately 0.64ha. P-1 accounts for the heavily wooded area to the west of the access road and conveys stormwater by sheet flow to the west property line and onto the neighboring property, this area will remain undeveloped.

Drainage area P-2 is approximately 3.87ha. P-2 encompasses a portion of the land east of the access road and conveys stormwater by sheet flow to the northwest corner of the property and into the existing quarry. There is a small portion of the adjacent property to the east that may drain to this area.

Drainage area P-3 is approximately 2.08ha. P-3 encompasses a portion of the land east of the access road and conveys stormwater by sheet flow to the southwest corner of the site and into an existing ditch that runs parallel to the access road for the quarry and ultimately drains into the ditch along Highway 2.

Pre-Development Runoff Values (m ³ /s)								
Area	2-Year	5-Year	10-Year	25-Year	100-Year			
P-1	0.23	0.36	0.45	0.58	0.78			
P-2	0.35	0.50	0.59	0.72	0.92			
P-3	0.19	0.27	0.32	0.39	0.49			

3.2 Post-Development Drainage Areas

During the design process QCA has been consulted on issues regarding post-development stormwater drainage area boundaries, TSS removal, and quantity and quality control. The site will be graded to ensure sheet flow towards the proposed swale and pond. A sketch of the proposed post-development drainage areas can be found in Appendix D.

Post-development area A-1 is 0.64ha and will consist of Pre-development area P-1. The area is heavily treed and will remain undeveloped.



Post-development area A-2 is 5.95ha and will consist of Pre-development areas P-2 and P-3. The site will be regraded so water will flow from the northern corner of the site to the southern corner where the pond will be located. Stormwater will be conveyed by sheet flow across the site where it will enter a flat-bottomed grassed swale, which will convey the flow directly into the pond. Perimeter swales will capture any sheet flow graded to the lot boundaries and direct to the southwest corner of the site.

3.3 Hydrologic & Hydraulic Modelling

The site was modelled using PC-SWMM (Version 7.3.3095) which is a hydrologic and hydraulic modelling software that uses EPA SWMM (Version 5.1.015). The software simulates the precipitation and runoff of watersheds.

3.3.1 Design Storms

The SCS Type II storm was chosen as the design storm for this model. The storm provides a peak intensity suitable for sizing conveyance methods and provides rainfall volumes that are suitable for sizing storage elements.

PCSWMM utilizes the Watershed lag method to determine the time of concentration for each sub-catchment area. The Watershed lag method uses the flow length, maximum potential retention and average watershed slope to calculate the time of concentration.

The Ontario Ministry of Transportation (MTO) Intensity-Duration-Frequency curve lookup tool was used to determine the rainfall hyetographs for storm events between the 2-year and 100-year return periods. The resulting hyetographs were used to calculate the total runoff for the pre-development and post-development area. The IDF tables can be found in Appendix B.

Runoff coefficients were taken from the MECP Stormwater Design Manual. Gravel was treated as asphalt to account for potential paving in the future.

Post-Development Unrestricted Runoff Values (m ³ /s)								
Area	25mm 4hr-Chicago	2-Year	5-Year	10-Year	25-Year	100- Year		
A-1	0.06	0.23	0.36	0.45	0.58	0.78		
A-2	0.59	0.85	1.18	1.41	1.71	2.16		

3.4 Stormwater Quantity Control

To achieve pre-development release rates the proposed development will restrict the release rate of stormwater runoff using an ICD. The pre-development release rate is calculated for a 2, 5, 25, and 100-year rainfall event. The storage pond is designed for retention of a 100-year rainfall event in accordance with common Best Management Practices (BMPs). The ICD will restrict the post-development release rates to 17% less than the pre-development release rates.

Stormwater leaving the wet pond will be controlled by a 300mm quality control orifice and a rectangular weir, for the quantity control. The orifice invert will be placed at the permanent pool elevation (122.20m). The orifice will control the 25mm, 2-year-10-year storms. The rectangular



weir will be set at the 10-year storm elevation (123.40m), and will control all storms greater than the 10-year storm. Calculations and a staged release summary from the orifice and weir can be found in Appendix C. The pond will have a permanent pool elevation of 122.20m, a maximum extended detention water level of 123.60 m and 0.3m of freeboard (123.90m). The proposed pond will provide a storage volume of 3259m³ and a peak 100-year controlled flow rate of 416L/s.

The discharge from the orifice and weir will flow down a riprap lined slope and into the grassed roadside ditch parallel to the existing access road. For more detailed information on the planned lot grading and overall project stormwater drainage plan please refer to drawing C101 in the design drawing set provided in Appendix F.

A-2 Post-Development Restricted Runoff and Storage (m ³ /s)						
Storm	Release Rate	Storage (m ³)				
25mm 4hr-Chicago	0.11	908.2				
2-Year	0.157	1707.5				
5-Year	0.183	2366.8				
10-Year	0.215	2615.8				
100-Year	0.416	3259.01				

3.5 Stormwater Quality Control

The quality requirements of "enhanced" 80% TSS removal will be achieved by using a wet pond. The pond was designed based on guidelines presented in MECP Stormwater Management Planning and Design Manual. Based on the MECP Design Manual the required storage volume per hectare is 250m³ per hectare. The area of the site contributing to the pond is 5.95 ha, giving a required volume of 1487m³.

To meet the MECP sizing guidelines and to reduce the release rate to less than predevelopment flow rates, the pond has been over sized. The pond will provide a permanent pool storage volume of 1523m³ and an active storage volume for the 25mm storm event of 908m³. The pond will have an active storage for the 100-year storm event of 3259m³. The maximum active storage height will be 1.4m with 0.3m of freeboard.

The pond's sediment forebay is designed to have a 2 to 1 length to width ratio and a 1.5-meterdeep permanent pool. This allows rate of the runoff to be reduced and allows time for sediment to settle. The forebay and permanent pool are separated by a rock flow check dam. The dam encourages pooling and reduces sediment from entering the permanent pool. The bottom of the pond has a permanent pool depth of 1.5m. Vegetation around the pond has been selected from the MECP guidelines and will aid in erosion control of the pond edge and deter waterfowl from entering the pond.

The entire development will employ Best Management Practices (BMPs) wherever possible. The intent of implementing stormwater BMPs throughout the development is to ensure that



water quality and quantity concerns are addressed at all stages of development. BMPs will be implemented at the lot, conveyance and end of pipe levels.

Lot level BMPs include the minimizing of ground slopes and maintaining as much of the lot as possible in a natural state. Recent recommendations by a number of Conservation Authorities and the MECP suggest that yard grading as flat as 0.5% be implemented to promote infiltration. The target range for finished ground slopes is recommended as 1.5% - 3% where possible for ease of grading. This range of slope will provide a significant opportunity for the absorption and filtration process in order to achieve a "normal" level of TSS removal. The side slope of all swales and drainage ditches shall not exceed 3:1. Side slopes steeper than 3:1 are prone to erosion and are difficult to maintain. In addition, swales are to be built with minimum depth and slope to allow for the opportunity for filtration and settlement of total suspended solids in grassed swales.

The conveyance methods to be utilized on the newly developed site are overland sheet flow and grassed swales directing flows to the new wet pond. All swales will be constructed at minimal gradient where possible, thus promoting absorption infiltration, as well as providing opportunity for particle filtration. Prior to construction heavy duty silt fence is to be installed around the proposed development and a straw bale check dam is also to be installed at the existing drainage channel outlet.

4.0 Maintenance

Occasional inspection and routine maintenance will be required to be carried out during construction and throughout the life of the stormwater system. The stormwater swales and storage pond are on private property. It will be the responsibility of the contractor to carry out routine visual inspections of the swale and storage pond during construction.

Once vegetation is established it will be the responsibility of the owner to carry out maintenance and inspections. Inspection of the stormwater swales and storage pond should be completed after each significant storm event for the first two years with quarterly inspection from then on. Inspections should include checking for sediment build up and vegetation health. Sediment removal is to be included with regular maintenance as well as replanting of any failed vegetation. Sediment removal should occur every 10 years. This will aid in the long-term performance of the stormwater swales and retention pond. It is recommended that all drainage swales be kept clear of debris.

Shoreline vegetation shall be maintained in a healthy state with weeds being removed on a regular basis. The outlet control device (rectangular weir) shall be inspected for deterioration yearly and maintained in good condition.

5.0 Summary

The proposed development of 8205 County Road 2, Napanee, will provide the required stormwater management control of post-development flows to pre-development level for the 2-year to 100-year storm events. The plan will require the construction of a wet storage pond to



provide runoff storage, detention, and discharge control using an orifice and a rectangular weir as an ICD. The stormwater management plan will utilize sheet flow and drainage swales to provide additional quality control measures that will achieve an "enhanced" level of TSS removal for all runoff from the site. Construction of erosion protection and sediment control will eliminate sediment laden runoff from leaving the site until vegetation is restored.

Report prepared by:

Daniel Fox, Engineering Technologist



Report Reviewed by:

Martin Burger, M.Eng., P.Eng.



Statement of Qualifications and Limitations

The attached Report has been prepared by Groundwork Engineering Limited (the Consultant) for the benefit of the Client in accordance with their Agreement.

The information, data, recommendations and conclusions contained in the Report:

- 1. is subject to the scope, schedule, and other constraints and limitations in the Agreement and the qualifications contained in the Report;
- 2. represents the Consultant's judgement in light of the limitations and industry standards for the preparation of similar reports;
- 3. may be based on information provided to Consultant which has not been independently verified;
- 4. has not been updated since the date of issuance of the Report and its accuracy is limited to the time and circumstances in which it was prepared; and
- 5. Must be read as a whole and sections should not be read out of context.

The Consultant shall be entitled to rely upon the accuracy and completeness of information that was provided to it and has no obligation to update such information. Consultant accepts no responsibility for any events or circumstances that may have occurred since the date on which the Report was prepared.

Any estimates or opinions regarding expected construction costs or construction schedule provided by Consultant represent Consultant's judgement in light of its experience and the knowledge and information available to it at the time of preparation. The Consultant does not make any representations, with respect to such estimates or opinions, and accepts no responsibility for any loss or damage arising from them. Persons relying on such estimates or opinions do so at their own risk.

Except as agreed to in writing by the Consultant and the Client; as required by-law; or to the extent used by governmental reviewing agencies for the purpose of obtaining permits or approvals, the Report and the Information may be used and relied upon only by the Client.

The Consultant accepts no responsibility, to parties other than the Client who may obtain access to the Report or the information for any injury, loss or damage suffered by such parties arising from their use of, reliance upon, or decisions or actions based on the Report, except to the extent those parties have obtained the prior written consent of the Consultant to use and rely upon the Report and the information. Any injury, loss or damages arising from improper use of the Report shall be borne by the party making such use.



Appendix A

Pre-Development Drainage Areas



			Groundwork
	l,		Engineering
	र		Limited
		GEOTECHNICAL • CIV	IL • STORMWATER • ONSITE WASTEWATER
		UNIT 64 Kin Off	0 - 654 NORRIS COURT IGSTON, ONTARIO FICE (613) 634-1789
			II Switzevi
PART 2			SUBJECT SITE
29R - 905(D2)		Surreumaan in Surreum Surreumaan in Surreumaan in	
23/(303(PZ)		Greater Napanee	
PIN 45116-0106(LT)		ndenativi South Napanë	
	/		and the second second
		2	
		45/10	Anderson by crassing present
\sim		LE	<u>GEND</u>
		2%	PROPOSED SLOPE
		84.19	EXISTING GRADE
		83.65	PROPOSED GRADE
/		\$165	EXISTING CONTOUR
			DRAINAGE SWALE
		ALL EXISTING GR	ADES TAKEN FROM TOPO SURVEY
		REVISIONS	
		No.	Description Date FOR SWM REPORT 2020/06/24
		#2 REVISED	D FOR SWM REPORT 2020/12/16
		##. XXX	XXX.XX
			3 Brughs
			Objince of ourse
		Client / Land Owner: TO	MLINSON GROUP
		Project: NAPA	NEE ASPHALT PLANT
		NAPANEE Drawing Title:	ONTARIO
		PRE-DEVEL	OPMENT DRAINAGE AREAS
		Drawn by: DF Checked By:	Project Number: GW-20019
		MB Page Size: 24"x36" Scale: 1.750	
		Date: JUNE 6, 2020	SHEET 1 of 1



Appendix B

MTO IDF Data

GEOTECHNICAL • CIVIL • STORMWATER • ONSITE WASTEWATER

www.groundengineer.ca

♂Ontario IDF CURVE LOOKUP

Active coordinate

44° 15' 15" N, 76° 56' 15" W (44.254167,-76.937500)

Retrieved: Wed, 09 Jan 2019 18:19:21 GMT



Location summary

These are the locations in the selection.

IDF Curve: 44° 15' 15" N, 76° 56' 15" W (44.254167,-76.937500)

Results

An IDF curve was found.





Coefficient summary

IDF Curve: 44° 15' 15" N, 76° 56' 15" W (44.254167, -76.937500)

Retrieved: Wed, 09 Jan 2019 18:19:21 GMT

Data year: 2010

IDF curve year: 2010

Return period	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Α	21.0	27.9	32.4	38.1	42.3	46.5
В	-0.699	-0.699	-0.699	-0.699	-0.699	-0.699

Statistics

Rainfall intensity (mm hr⁻¹)

Duration	5-min	10-min	15-min	30-min	1-hr	2-hr	6-hr	12-hr	24-hr
2-yr	119.3	73.5	55.3	34.1	21.0	12.9	6.0	3.7	2.3
5-yr	158.5	97.6	73.5	45.3	27.9	17.2	8.0	4.9	3.0
10-yr	184.0	113.4	85.4	52.6	32.4	20.0	9.3	5.7	3.5
25-yr	216.4	133.3	100.4	61.9	38.1	23.5	10.9	6.7	4.1
50-yr	240.3	148.0	111.5	68.7	42.3	26.1	12.1	7.4	4.6
100-yr	264.1	162.7	122.5	75.5	46.5	28.6	13.3	8.2	5.0

Rainfall depth (mm)

Duration	5-min	10-min	15-min	30-min	1-hr	2-hr	6-hr	12-hr	24-hr
2-yr	9.9	12.2	13.8	17.0	21.0	25.9	36.0	44.4	54.7
5-yr	13.2	16.3	18.4	22.6	27.9	34.4	47.8	58.9	72.6
10-yr	15.3	18.9	21.3	26.3	32.4	39.9	55.6	68.5	84.3
25-yr	18.0	22.2	25.1	30.9	38.1	46.9	65.3	80.5	99.2
50-yr	20.0	24.7	27.9	34.3	42.3	52.1	72.5	89.4	110.1
100-yr	22.0	27.1	30.6	37.7	46.5	57.3	79.7	98.2	121.0

Terms of Use

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Appendix C

Stormwater Management Calculation Sheets



Stormwater Wetpond Design Calculation

Project Name : Project Address : Prepared By: Napanee Asphalt Plant 8205 Highway 2, Napanee Daniel Fox Project Number: Clients Name : Reviewed By: GW-20019 Tomlinson Group Martin Burger

Sediment Forebay Design

	Calculation Variables	Settling Calculation				
2	r = Length to Width Ratio	Diet	_	r Q _p	r= Q _p = V. =	2 0.52
0.52	Q _p = Peak Flow Rate For Design Storm (10Yr Storm)	Dist =		\bigvee V _s	۰s	0.0005
0.0003	V_s = Settling Velocity (0.0003 m/s)	Settling Length			58.88 n	า
0.55	Q = Inlet Flow Rate(m ³ /s) (25mm Storm)	Dispersion Length				
1.5	d = Depth of Permanent Pool (m)	Dist	_	<u>8Q</u>	Q = d = V ₆ =	0.55 1.5 0.4
0.4	V _f = Desired Forebay Velocity (m/s)			$d V_{f}$	ľ	•
			ersion L	ength	7.33 n	า
		Minimum Forebay Width				
		Widtl	h =	Dist 8	Dist=	58.88

Forebay Deep Zone Width 7.36 m



Stormwater Wetpond Design Calculation

Project Name : Project Address : Prepared By: Napanee Asphalt Plant 8205 Highway 2, Napanee Daniel Fox Project Number: Clients Name : Reviewed By: GW-20019 Tomlinson Group Martin Burger

Storage Requirements

Required TSS Removal
SWMP Type
Impervious Level
Site Area In Hectares
Required Storage Volume Per

Water Quality Storage Requirements							
		35%	55%	70%	85%		
	Infiltration	25	30	35	40		
Enhanced 80%	Wetlands	80	105	120	140		
Ellianceu 80%	Hybrid Wet Pond/Wetland	110	150	175	195		
	Wetpond	140	190	225	250		
	Infiltration	20	20	25	30		
Nermal 70%	Wetlands	60	70	80	90		
Normal 70%	Hybrid Wet Pond/Wetland	75	90	105	120		
	Wetpond	90	110	130	150		
	Infiltration	20	20	20	20		
	Wetlands	60	60	60	60		
Basic 60%	Hybrid Wet Pond/Wetland	60	70	75	80		
	Wetpond	60	75	85	95		
	Dry Pond	90	150	200	240		

Required Volume	1487.5 m ³	
Permanent Pool Volume	1249.5 m ³	
Active Storage Volume	238 m ³	

Stage Storage Discharge

Water Surface		Incromontal	Intromontal		Quality Control	Invert of Orifice	Contarling of Orifica	Head Loss Across			
Elevation (m)	Area (m2)	Dopth (m)	Volumo (m2)	Total \ (aluma (m2)	Quality Control	Elevation	Elevation (m)	Orifico (m)	Delesse Dete	Natas	
	Area (mz)		volume (ms)	Total Volume (m3)	Office diameter				Release Rate	Notes	
122.20	0	0.05	0	0	0.30	122.20	122.350	0	0.000	orifice	
122.25	1654.66	0.05	82.73	82./3	0.30	122.20	122.350	-0.10	#NUM!	orifice	
122.30	1617.55	0.05	80.88	163.61	0.30	122.20	122.350	-0.05	#NUM!	orifice	
122.35	1670.84	0.05	83.54	247.15	0.30	122.20	122.350	0.00	0.0000	orifice	
122.40	1724.52	0.05	86.23	333.38	0.30	122.20	122.350	0.05	0.0420	orifice	
122.45	1778.59	0.05	88.93	422.31	0.30	122.20	122.350	0.10	0.0594	orifice	
122.50	1833.05	0.05	91.65	513.96	0.30	122.20	122.350	0.15	0.0728	orifice	
122.55	1887.91	0.05	94.40	608.36	0.30	122.20	122.350	0.20	0.0840	orifice	
122.60	1943.16	0.05	97.16	705.51	0.30	122.20	122.350	0.25	0.094	orifice	
122.65	1998.79	0.05	99.94	805.45	0.30	122.20	122.350	0.30	0.103	orifice	
122.70	2054.83	0.05	102.74	908.20	0.30	122.20	122.350	0.35	0.111	<mark>25mm</mark> orifice	
122.75	2111.26	0.05	105.56	1013.76	0.30	122.20	122.350	0.40	0.119	orifice	
122.80	2168.07	0.05	108.40	1122.16	0.30	122.20	122.350	0.45	0.126	orifice	
122.85	2225.29	0.05	111.26	1233.43	0.30	122.20	122.350	0.50	0.133	orifice	
122.90	2282.89	0.05	114.14	1347.57	0.30	122.20	122.350	0.55	0.139	orifice	
122.95	2340.89	0.05	117.04	1464.62	0.30	122.20	122.350	0.60	0.146	orifice	
123.00	2399.28	0.05	119.96	1584.58	0.30	122.20	122.350	0.65	0.151	orifice	
123.05	2458.06	0.05	122.90	1707.48	0.30	122.20	122.350	0.70	0.157	2-YEAR orifice	
123.10	2517.23	0.05	125.86	1833.34	0.30	122.20	122.350	0.75	0.163	orifice	
123.15	2576.8	0.05	128.84	1962.18	0.30	122.20	122.350	0.80	0.168	orifice	
123.20	2636.76	0.05	131.84	2094.02	0.30	122.20	122.350	0.85	0.173	orifice	
123.25	2697.12	0.05	134.86	2228.88	0.30	122.20	122.350	0.90	0.178	orifice	
123.30	2757.86	0.05	137.89	2366.77	0.30	122.20	122.350	0.95	0.183	5-Year orifice	
123.35	2818.99	0.05	140.95	2507.72	0.30	122.20	122.350	1.00	0.188	orifice	
123.40	2880.53	0.05	144.03	2651.75	0.30	122.20	122.350	1.05	0.215	10-YEAR orifice	
123.45	2942.46	0.05	147.12	2798.87	0.30	122.20	122.350	1.10	0.220	Orifice and wei	eir
123.50	3004.77	0.05	150.24	2949.11	0.30	122.20	122.350	1.15	0.265	Orifice and wei	eir
123.55	3067.48	0.05	153.37	3102.48	0.30	122.20	122.350	1.20	0.323	Orifice and wei	eir
123.60	3130.58	0.05	156.53	3259.01	0.30	122.20	122.350	1.25	0.416	100-YEAR Orifice and wei	eir



Appendix D

Post-Development Drainage Areas



			Groundwork	
			Engineering	a
			Limited	9
<u>s</u>		GEOTECHNICAL • CIVI		ATER
		UNIT 64	0 - 654 NORRIS COURT	
		KIN OFF	IGSTON, ONTARIO FICE (613) 634-1789	
			LOCATION F	LAN
		1 17 11		K
PART 2		-Roll Insumations	SUBJECT SITE	
$29R - 905(P_2)$		surface and the second se		
		Greater Napanee		4
PIN 45116-0106(LT)		ungest N South Napan e		
	-			Die Colore Boltz
		2		F+
			Anderson	amonat
~//				
		 2%	PROPOSED SLOPE	
		84 19	EXISTING GRADE	
		83.65	PROPUSED GRADE	
			EXISTING CONTOUR	
			DRAINAGE SWALE	
		ALL EXISTING GR	ADES TAKEN FROM TOPO SURVEY	
		REVISIONS No.	Description Da	ate
		#1 ISSUED #2 REVISED	FOR SWM REPORT 2020/ D FOR SWM REPORT 2020/	/06/24 /12/16
		BENCHMARK: No. DESCRIPTIO	N ELEVATION	44
		##. XXX	XXX.XX M. H. BURG	ER
			3 Down	De la
			NUCE OF O	NI
		Client / Land Owner:	MLINSON GROUP	
		Project: NAPA	NEE ASPHALT PLANT	
		NAPANEE Drawing Title:	10	NTARIO
		POST DEVE	LOPMENT DRAINAGE AREAS	
		Drawn by: DF	Project Number:	2
		Page Size: 24"x36"	Drawing Number:	
		Scale: 1:750 Date: JUNE 6, 2020	SHEET 1 of 1	



Appendix E

Design Drawing Set



- SURVEY DATA SHOWN ON THIS PLAN ARE SUPPLIED FOR INFORMATION PURPOSES ONLY. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THE ACCURACY OF ALL INFORMATION OBTAINED PRIOR TO CONSTRUCTION. IF THERE IS ANY DISCREPANCY THE CONTRACTOR IS TO NOTIFY THE ENGINEER PROMPTLY.
- LOCATION, SIZE, MATERIAL AND ELEVATIONS OF ALL EXISTING UTILITIES PRIOR TO COMMENCING CONSTRUCTION. PROTECT AND ASSUME ALL RESPONSIBILITY FOR EXISTING UTILITIES WHETHER OR NOT SHOWN ON THE DRAWINGS. IF THERE ARE ANY DISCREPANCIES THE CONTRACTOR IS TO NOTIFY THE ENGINEER PROMPTLY. GAS, HYDRO, CABLE,
- ACCORDANCE WITH ONTARIO PROVINCIAL STANDARDS AND
- BETTER UNLESS OTHERWISE SPECIFIED. ANY GRASSED AREAS SEED.
- PURPOSES.

- TO 1 VERTICAL).
- OF STONE 150MM-300MM, NO FINES. RIP RAP TO BE PLACED ON NON-WOVEN GEOTEXTILE (TEARAFIX 270R) OR EQUIVALENT
- AND 802.013 UNLESS NOTED OTHERWISE.
- TO MINIMUM 98% STANDARD PROCTOR DRY DENSITY. CLEAR STONE BEDDING SHALL NOT BE PERMITTED
- GEOTECHNICAL ENGINEER
- "A".
- PAVEMENT SUBGRADE TO 2 METRES BELOW FINISHED GRADE) SHALL MATCH EXISTING SOIL CONDITIONS.

- CONFORM TO OPSS MUNI 1850.
- GRATE.
- AND SITE WORKS COMPLETED.
- THE SITE OR INTO WATER BEARING FEATURES PRIOR TO ANY REINSTATED.
- SHALL BE NOTIFIED IMMEDIATELY.

- WELLS OR AS ADVISED;
- OF GANANOQUE ENVIRONMENT DEPARTMENT;



